

No. 10-03-03-04/02

SYSTEM: Space Shuttle RSRM 10 CRITICALITY CATEGORY: 1 SUBSYSTEM: Ignition Subsystem 10-03 PART NAME: Initiator Propellant (1) ASSEMBLY: Initiator Assembly 10-03-03 PART NO.: (See Table A-3) FMEA ITEM NO.: 10-03-03-04 Rev N Boost (BT) PHASE(S): CIL REV NO.: (See Table A-3) QUANTITY: DATE: 27 Jul 2001 EFFECTIVITY: (See Table 101-6) HAZARD REF.: BI-03 SUPERSEDES PAGE: 425-1ff. 31 Jul 2000 DATED: CIL ANALYST: F. Duersch APPROVED BY: DATE: RELIABILITY ENGINEERING: K. G. Sanofsky 27 July 2001 V. B<u>. Teller</u> ENGINEERING: 27 July 2001 1.0 FAILURE CONDITION: Failure to operate (B) 2.0 FAILURE MODE: 1.0 Failure to ignite 3.0 FAILURE EFFECTS: No ignition on one RSRM, causing thrust imbalance and loss of RSRM and loss of SRB, crew, and vehicle 4.0 FAILURE CAUSES (FC): FAILURE CAUSE KEY FC NO. DESCRIPTION Low ignitability of propellant 1.1 1.1.1 Propellant contamination Α 1.1.2 В Propellant grain surface contamination 1.1.3 Ammonium Perchlorate (AP) leaching С 1.1.4 Improper mixing of materials D 1.1.5 Nonconforming raw materials Ε 1.1.6 F Improper formulation 1.2 Moisture/high humidity 1.2.1 Initiator nozzle seals improperly installed G 1.2.2 Moisture/high humidity during processing Н

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5.0 REDUNDANCY SCREENS:

SCREEN A: N/A SCREEN B: N/A SCREEN C: N/A

6.0 ITEM DESCRIPTION:

- Initiator propellant is designated TP-H1178 and is composed of bimodal ammonium perchlorate (AP) oxidizer, spherical aluminum, ferric oxide, polybutadiene acrylic acid acrylonitrile HB polymer binder, and Epoxy Curing Agent (ECA).
- The initiator casting process is designed to ensure the propellant grain configuration is free of foreign materials and objects. The initiator propellant grain configuration is a 30-point star web grain design. Star peaks and valleys are rounded to reduce the likelihood of stress discontinuities (Figures 1 and 2). After casting is completed and core removed, the initiator is inspected for cracks or voids.
- Initiator propellant is up to peak thrust in 0.02 seconds and the main igniter is up to 90 percent of peak output by 0.045 seconds from time zero. The flame from the igniter exhausts onto the forward star of the forward segment and ignites this surface initially. Ignition of the rest of the propellant surface occurs very rapidly. RSRM internal pressure increases rapidly and achieves lift-off thrust in less than 0.3 seconds.
- Initiator propellant is protected from atmospheric exposure by initiator seal discs bonded over the initiator nozzle inserts. Seals protect the loaded initiator from propellant degradation due to moisture or humidity. The seals are bonded into the initiator nozzle holes with asbestos float-filled epoxy sealant. The initiator is further protected from moisture and humidity by the inner gasket, packing with retainers, initiator nozzle port environmental seals, and Barrier-Booster seals. An igniter protective cover is required to seal the Safety and Arming (S&A) device attachment flange on the igniter adapter. The protective cover is temporary until the S&A device is installed at KSC. The cover is made of aluminum and has an O-ring seal.
- Each lot of propellant raw materials is standardized per engineering to meet burn rate and mechanical property requirements. Materials are listed in Table 1.

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TABLE 1. MATERIALS

Drawing No.	Name	Material Material	Specification	Quantity
	Propellant	TP-H1178	STW5-2833	A/R
	·	Terpolymer (PBAN)	STW4-2600	A/R
		Liquid Epoxy Resin	STW4-2601	A/R
		Ammonium Perchlorate		
		with Conditioner	STW4-2602	A/R
		Ferric Oxide	STW4-2604	A/R
		Aluminum, Spherical	STW4-2832	A/R

The above materials make up TP-H1178 propellant which is used in the following parts:

1U77858 1U77372	Igniter Initiator Chamber, Loaded Igniter Chamber, Loaded						
	Sealant	Liquid Epoxy Resin,					
		Ashestos Float-Filled	STW5-2678	A/R			

6.1 CHARACTERISTICS

- Initiator propellant is designated as TP-H1178 and is composed of bimodal Ammonium Perchlorate (AP) oxidizer, spherical aluminum, ferric oxide, polybutadiene acrylic acid acrylonitrile HB polymer binder, and Epoxy Curing Agent (ECA).
- The initiator propellant grain configuration is a 30-point star web grain design. Star peaks and valleys are rounded to reduce the likelihood of stress discontinuities (Figures 1 and 2).

7.0 FAILURE HISTORY/RELATED EXPERIENCE:

Current data on test failures, flight failures, unexplained failures, and other failures during RSRM ground processing activities can be found in the PRACA Database.

8.0 OPERATIONAL USE: N/A

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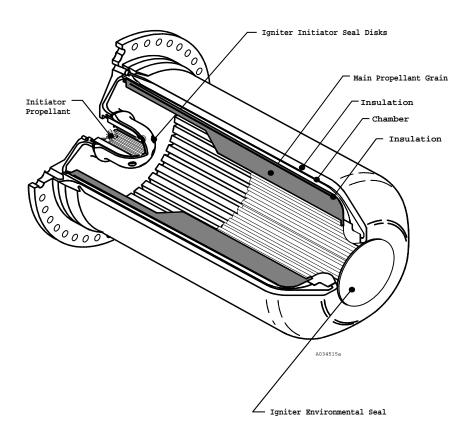


Figure 1. Igniter and Initiator Propellant Grain Configurations

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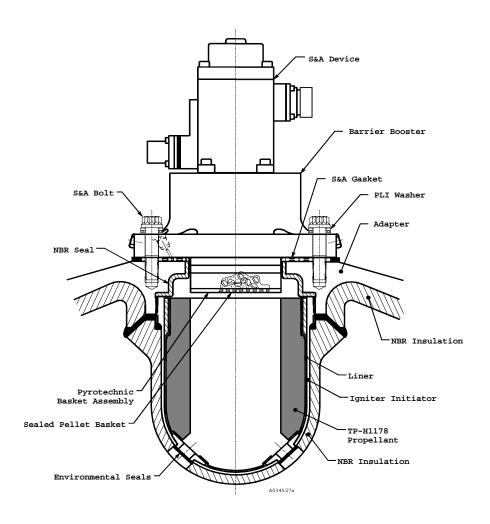


Figure 2. Loaded Igniter Initiator

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RATIONALE FOR RETENTION: 9.0

9.1 DESIGN:

DCN FAILURE CAUSES

A,B	1.	Propellant raw materials have storage life from date of manufacture when stored at warehouse ambient conditions in unopened containers or containers that were resealed after each use. The storage life expiration date of an individual lot of material may be extended provided the material satisfactorily passes retest requirements. Contamination control requirements and procedures are described in TWR-16564. During propellant processing, temperature, moisture, humidity, and
		contamination are controlled per engineering drawings and shop planning for the

Terpolymer (HB) a.

following materials:

- Epoxy resin b.
- Ammonium Perchlorate (AP) C.
- d. Spherical aluminum
- Ferric Oxide, Type I e

A,B	2.	Igniter	initiator	nozzle	seals	provide	protection	against	contamination	after	the
		initiato	r is asser	nbled.							

- A,BManufacturing processes for initiator propellant are per engineering and shop planning.
- The igniter initiator shipping configuration includes an end cover to provide A.B protection against contamination during shipping and storage.
- Design engineering reviews, analyzes, and publishes results of 5-inch CP and Lot A,B,D,E,F 5. Acceptance Tests (LAT) per engineering.
- A.B 6. Mechanical properties data from an aging test of TP-H1178 propellant indicate allowable stresses, strains, and elastic modulus are not affected by aging per TWR-19292.
- C,G,H The igniter environmental seal is cured acrylonitrile butadiene rubber (NBR) which conforms to material properties per engineering. The seal is bonded over the igniter nozzle with an asbestos float-filled liquid epoxy resin sealant that contains a polyamide curing agent and a thixotropic agent. The environmental seal protects loaded igniter and initiator propellant from degradation due to exposure to moisture and humidity per engineering drawings and specifications.
- C,G,H Delta qualification temperature and humidity testing of loaded igniter assemblies with environmental seals in place showed no propellant performance degradation per TWR-12310 and TWR-12323.
- C.G.H Initiator environmental seals are discs of cured asbestos and silicon dioxide-filled NBR. The seals are bonded over the initiator openings with a sealant. The seals protect the loaded initiator and igniter from propellant degradation due to exposure to moisture and humidity. The initiator is further protected from moisture and humidity by the inner gasket, packing with retainers, igniter environmental seal, and Barrier-Booster seals per engineering drawings.
- 10. An igniter protective cover is required to seal the S&A attachment flange on the C.H igniter adapter. The cover is made of aluminum and has an O-ring seal per engineering drawings.

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C.G.H

D,F

D

Ε

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С 11. Moisture, high humidity, and temperature conditions are maintained within limits during AP storage and during propellant mixing operations per engineering

drawings and shop planning.

12. Sealant raw material specifications are defined in engineering for the following

materials:

Asbestos float a.

- Liquid epoxy resin b.
- Polyamide curing agent C.
- Microfine silicon dioxide

D.F 13. Propellant mix proportions and mechanical property requirements of Igniter/Initiator Propellant (TP-H1178) are per engineering.

14. Fine adjustment for percent of ground AP, (HB) polymer, and ECA proportions are determined by standardization per engineering to meet burn rate requirements and propellant mechanical properties. Average burn rate of 5-inch Center Perforated (CP) motors is used to adjust percent ground oxidizer content which adjusts the burn rate. Liquid Strand Burn Rate (LSBR) of standardization batches is used to determine the target burn rate of production propellant batches. Tests on loaf samples are processed to determine propellant mechanical properties. Propellant standardization is the process of determining the percentages of raw materials that will produce desired propellant physical and ballistic properties of production

batches per engineering.

D 15. Raw material weighing is per engineering drawings and specifications.

16. Propellant processing, mixing, and cure requirements are per engineering and

shop 'planning.

17. Raw material conformance specifications, material properties requirements, and means of verification for TP-H1178 propellant are established per engineering for

the following materials:

Terpolymer (HB) a.

- Epoxy resin b.
- Ammonium Perchlorate C.
- Spherical aluminum d.
- Ferric Oxide, Type I

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9.2	TEST AN	D INS	SPEC	ION:		
<u>DCN</u>	FAILURE TESTS	CAU (T)	SES	nd		CIL CODE
			1.	For New HB Polymer, verify:		
	E E E E E E E E A,B,E	(T) (T) (T) (T) (T) (T) (T) (T)		 a. Acid number b. Acrylonitrile content c. Agerite stalite content d. Cetyldimethyl benzyl ammonium chloride content e. Chloride f. Unbound/total acid ratio g. Infrared spectrum h. Iron content i. Moisture content j. No shipping or handling damage k. Viscosity l. Workmanship shall be such that the HB polymer is light to dark amber/brown in color, that may contain particulates 	in small visible	06,ALC009 11,ALC014 16,ALC019 21,ALC024 26,ALC029 31,ALC034 36,ALC039 41,ALC045 ALC046
			2.	For New Liquid Epoxy Resin verify:		
	C,E,G,H C,E,G,H C,E,G,H E C,E,G,H C,E,G,H C,E,G,H A,B	(T) (T) (T) (T) (T) (T)		 a. Hydrolyzable chlorine percent b. Infrared spectrum c. Moisture percent d. No shipping or handling damage e. Specific gravity f. Viscosity g. Weight per epoxy h. Workmanship is uniform in appearance and free frecontamination 	ALD006,ALD0 ALD035,ALD0 ALD061,ALD0 ALD082,ALD0 ALD098,ALD1 rom visible	ALD030 38,ALD042 ALD052 63,ALD068 85,ALD091
			3.	For New Ammonium Perchlorate, verify:		
	E E E E E E E E E E E E E E E E E E E	EEEEEEE EEEEEE		a. Acid insolubles b. Bromate c. Bulk density d. Chlorate e. Chloride f. External moisture content g. Internal moisture content h. Iron i. No shipping or handling damage j. Particle size distribution k. Assay, as ammonium perchlorate l. pH m. Phosphate n. Photomicrographic analysis o. Sulfated ash p. Total moisture content q. Workmanship is uniform in appearance and free for	ALE001,ALE0 ALE007,ALE0 ALE012,ALE0 ALE017,ALE0 ALE022,ALE0 ALE033,ALE0 ALE038,ALE0 ALE045,ALE0 ALE052,ALE0 ALE058,ALE0 ALE063,ALE0 ALE068,ALE0 ALE091,ALE0	008,ALE011 113,ALE016 118,ALE020 123,ALE026 129,ALE032 134,ALE037 139,ALE042 ALE044 146,ALE050 155,ALE056 159,ALE062 164,ALE067 169,ALE072 192,ALE095
			4.	For New Ferric Oxide, verify:		
	E	(T)		a. Calcination loss	ALG0	00,ALG001

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E	(T)		b.	Iron content	AL	G010,ALG012
E E	(T)		c. d.	No shipping or handling damage Specific surface area		ALG019 G031,ALG032
A,B,E	(T)		e.	Workmanship is uniform in appearance and free fr contamination		ALG040
E	(T)	_	f.	Volatile loss	AL	G049,ALG050
		5.	For	New Aluminum, Spherical, verify:		
E E	(T) (T)		a. b.	Active spherical aluminum Iron content		.U001,ALU004 .U011,ALU014
F	` ,		C.	No shipping or handling damage	,	ALF011
E E	(T)		d.	Magnesium content	ΔΙ ΠΟ15 ΔΙ	.U016,ALU019
Ē	(T)		e.	Particle size distribution		.U021,ALU024
A,B	(1)		f.	Workmanship uniform in appearance and free fron		.0021,AL0024
А,Б			1.		II VISIDIC	A1 11004
_	(T)			contamination	41.11000.41	ALU034
Е	(T)		g.	Volatile matter	ALU036,AL	.U037,ALU040
		6.	For	New Propellant, SRM, Igniter verify:		
A,B,D,F A,B,D,F			a.	Acceptability of AP during oxidizer preparation Cleanliness and acceptability of facility during oxid	:	AOW008
А,Б,Д,Г			b.		izei	A () () () ()
4 D D E			_	preparation prior to grinding	.:	AOW009
A,B,D,F			C.	Cleanliness and acceptability of tote bins during ox	daizer	4.014/040
				preparation prior to grinding		AOW016
A,B,D,F			d.	Actual temperature of heated water during propella		AOW024
A,B,D,F			e.	All containers are free from moisture, contamination	n, and foreign	
				objects during premix preparation	,	AOW028
A,B,D,F			f.	All equipment is free from moisture, contamination	and foreign	7.0020
71,0,0,1			١.	objects during premix preparation	, and foreign	AOW030
D,E,F			g.	Spherical aluminum plus Ferric Oxide production b	atches,	AOW030
				uncured propellant		AOW052
D,F			h.	Spherical aluminum properly conditioned during pr	emix preparation	AOW065
A,B,D,F			i.	AP conditioning during oxidizer preparation	- P - P	AOW067
A,B,D,F			j.	AP conditioning requirement met during propellant	nrocessing	AOW068
						A0111000
A,B,D,F			k.	AP spillage weight is within allowable limits during mixing operations	propellant	AOW077
A,B,D,F			I.	AP stock and lot numbers comply with batch card	during	7.017011
				propellant processing		AOW080
A,B,D,F			m.	Cleanliness of mixing facility prior to mixing		AOW092
D,F			n.	ECA properly conditioned during premix preparation	n	AOW128
A,B,D,F			0.	End of mix temperature requirement met during pro		
D,E,F				Ground oxidizer particle size distribution production		AOW134
			p.			AOW 134
D,F			q.	Ground oxidizer particle size distribution sampling	requirements	4 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
				met during oxidizer preparation		AOW140
D,F			r.	HB polymer properly conditioned during premix pre	eparation	AOW 145
A,B,D,E,I	F (T)		S.	LSBR production batches, uncured propellant		AOW 154
D,F			t.	Mill load setting acceptable during oxidizer prepara	ation	AOW 167
A,B,D,F			u.	No lumps in propellant during propellant processin		AOW169
D,E,F			٧.	Oxidizer content production batches, uncured prop		AOW172
D,E,F			w.	Percent HB polymer production batches, uncured property		AOW182
						A011 102
A,B,D,F			Χ.	Premix constituent weights comply with batch card	uuririg	A () \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
D.F.				propellant processing	antina an alcondino	AOW190
D,F			у.	Premix constituents lot numbers are per shop plan	ning auring	
				premix preparation		AOW191
A,B,D,F			Z.	Premix constituents stock and lot numbers comply		AOW 193
A,B,D,F			aa.	Propellant samples taken after propellant mixing fr	om different	
				locations in the mix bowl		AOW207

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	ם כ			ah	Ciava analysis tost during avidizer proparation	A ()\A/210		
	D,F				Sieve analysis test during oxidizer preparation	AOW210		
	A,B,D,F	(T)		ac.	Stock and lot number of AP during oxidizer preparation	AOW216		
	D,E,F	(T)			Strain at maximum stress production batches	AOW218		
	D,E,F	(T)			Maximum stress production batches	AOW228		
	A,B,D,F			af.	Total oxidizer mixing time requirement during propellant processing	AOW238		
	D,E,F			ag.	Total solids production batches, uncured propellant	AOW243		
	D,F			ah.	Weight of spherical aluminum in bowl meets requirements during premix preparation	AOW258		
	D,F			ai.	Weight of AP spillage does not exceed maximum allowable limits during oxidizer preparation	AOW262		
	D,F			aj.	Weight of ECA meets weight requirements during premix preparation	AOW263		
	D,F				Weight of ground AP during oxidizer preparation	AOW265		
	A,B,D,F			al.	Weight of ground AP complies with batch card during propellant			
	D.F.				processing	AOW267		
	D,F D,F						Weight of HB polymer in bowl during premix preparation Weight of iron oxide in mix bowl meets weight requirements	AOW268
					during propellant premix preparation	AOW274		
	D,F				Weight of unground AP during oxidizer preparation	AOW275		
	A,B,D,F			ар.	Weight of unground AP complies with batch card during propellant processing	AOW277		
	D,F			aq.	Total AP weight (ground plus unground) meets allowable limits	AOWZII		
	D,1			aq.	during oxidizer preparation	AOW279		
			7.	For N	New Chamber Assembly, Igniter Initiator-Loaded verify:			
	C,G,H			a.	Area where environmental seals are to be bonded is cleaned with			
	-,-,				a swab dampened with approved solvent	AAM006		
	A,B,D,F			b.	Tooling and initiator chamber surfaces are clean and dry prior to			
	,- ,- ,-				liner application	AAM014		
569	C,G,H			C.	Sealant is acceptable and within pot life per planning	A N A L 10 4 7		
	005			لم	requirements	AMU017		
	C,G,F			d.	Each loaded initiator assembly for general condition and properly	A A N 400E		
	ССГ			_	packaged prior to shipping to stores	AAM025		
	C,G,F			e.	Initiator nozzle inserts correctly installed into initiator chamber	A A M 4022		
	C,G,F			f	nozzle ports	AAM032		
	C,G,F			f.	Initiator nozzle seals correctly installed into initiator chamber	A A B 4000		
	C,G,F			~	nozzle ports Initiator seal dimensions after fabrication	AAM033 AAM035		
				g.		AAW050		
	A,B,D,F			h.	Tooling is clean and dry prior to tooling dry-fit Each initiator in the lot is cast in one production run from the	AUWUSU		
	A,B			I.	same propellant mix and identified with propellant mix number			
					per the engineering drawing	AAM065		
	C,G,H			i	Proper removal of excess sealant	AAM073		
	C,G,H	(T)		J. k.	Shore A hardness tests of sealant	AAM077		
	A,B,D,F	(1)		r. I.	All tooling and liner are clean and dry immediately prior to casting	AAIVIOTT		
	۸,۵,۵,۱			1.	per shop planning	AOW089		
			8.	Ear N	Now 5 inch CP Ignitar Propollant, varify:			
			Ο.	i-Oi l'	New 5-inch CP, Igniter Propellant, verify:			
	A,B,D,E,F	(T)		a.	5-inch CP motor test data for propellant standardization and burn	A 0)A(000		
					rate per engineering	AOW000		
			9.	For N	New Igniter Assembly verify:			
	C,G,H			a.	Protective cover installed over S&A port prior to shipping of	A LL 1000		
	ССЦ			h	igniter assembly	AHJ003		
	C,G,H A,C,D,E,			b.	Propellant surface is free from AP leaching	AAM004		
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	F,G,H,	(T)		c. Initiator LAT for proper propellant burn time and presigniter specification	sure per the	AKU021
			10.	For New Floats, Asbestos verify:		
	C,G,H C,G,H C,G,H C,G,H C,G,H	(T) (T) (T) (T) (T)		 a. Calcination loss b. Fiber size distribution c. pH (aqueous extract) d. Volatile matter e. Wet volume 		ALI002 ALI011 ALI023 ALI051 ALI053
			11.	For Retest Floats, Asbestos verify:		
	C,G,H	(T)		a. Volatile matter for storage life extension		ALI051A
			12.	For New Curing Agent, Polyamide Liquid Resin, verify:		
	C,G,H C,G,H C,G,H C,G,H C,G,H	(T) (T) (T) (T) (T)		 a. Amine value b. Ash content c. Color d. Specific gravity e. Viscosity 	ALQ02	01,AMQ006 AMQ015 26,AMQ028 AMQ033 49,AMQ050
			13.	For New Silicon Dioxide, verify:		
	C,G,H C,G,H C,G,H C,G,H	(T) (T) (T) (T)		a. Bulk densityb. Loss on ignitionc. Moistured. pH	ALPO	02,ALP008 ALP040 058,ALP064 097,ALP101
			14.	For New NBR, verify:		
	C,G,H C,G,H C,G,H C,G,H C,G,H C,G,H	(T) (T) (T) (T) (T) (T)		 a. Elongation (calendered only) b. Mooney viscosity (extrusions only) c. Scorch characteristics (extrusions only) d. Shore A hardness (calendered only) e. Specific gravity (calendered only) f. Tensile strength (calendered only) g. Material workmanship including uniform appearance from contamination 	ALH010,ALH0 ALH041,ALH0 ALH081,ALH0 ALH098,ALH1 ALH118,ALH1 ALH147,ALH1 and free	46,ALH170 86,ALH171 02,ALH109 21,ALH126
			15.	For Retest NBR, verify:		
	C,G,H C,G,H	(T) (T)		a. Mooney viscosityb. Scorch characteristics		ALH049 ALH087
			16.	For New Segment, Rocket Motor, Forward, verify:		
	B,C,H			a. S&A shipping cover is installed prior to igniter installed	ation	LHA319
			17.	KSC verifies:		
5	C,G,H C,G,H			 a. Integrity of the S&A device and S&A gasket installati by high- and low-pressure leak test per OMRSD File Vol I, B47SA0.110 b. Igniter seal disk is free from punctures, debonds, or 	V,	OMD072
	5,5,11			that the disk is still sealed and intact and has no visil penetrations, debonds, or cracks per OMRSD, File V	ole	

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DATE: 27 Jul 2001 No. 10-03-03-04/02 SUPERSEDES PAGE: 425-1ff. DATED: 31 Jul 2000 B47SG0.020 OMD075 C,G,H Prior to final assembly of motor that the S&A device port protection cover is intact and undamaged per OMRSD, File V, Vol I B47SG0.100 OMD083 C,G,H Initiator is free from the following per OMRSD, File V, Vol I B47SG0.111: OMD084 Surface condition where white crystals are present 2. 595 Broken fins shall not exceed 1.7 inches 3. Moisture

4. AP leaching

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